U. S. DEPARTMENT OF COMMERCE NATIONAL OCEANIC AND ATMOSPHERIC ADMINISTRATION NATIONAL WEATHER SERVICE

NOAA Technical Memorandum NWSTM PR-19

A PROGRAM TO COMPUTE TURBULENCE
IN THE VICINITY OF LEE WAVES DOWNSTREAM OF SELECTED MOUNTAINS
IN THE HAWAIIAN ISLANDS

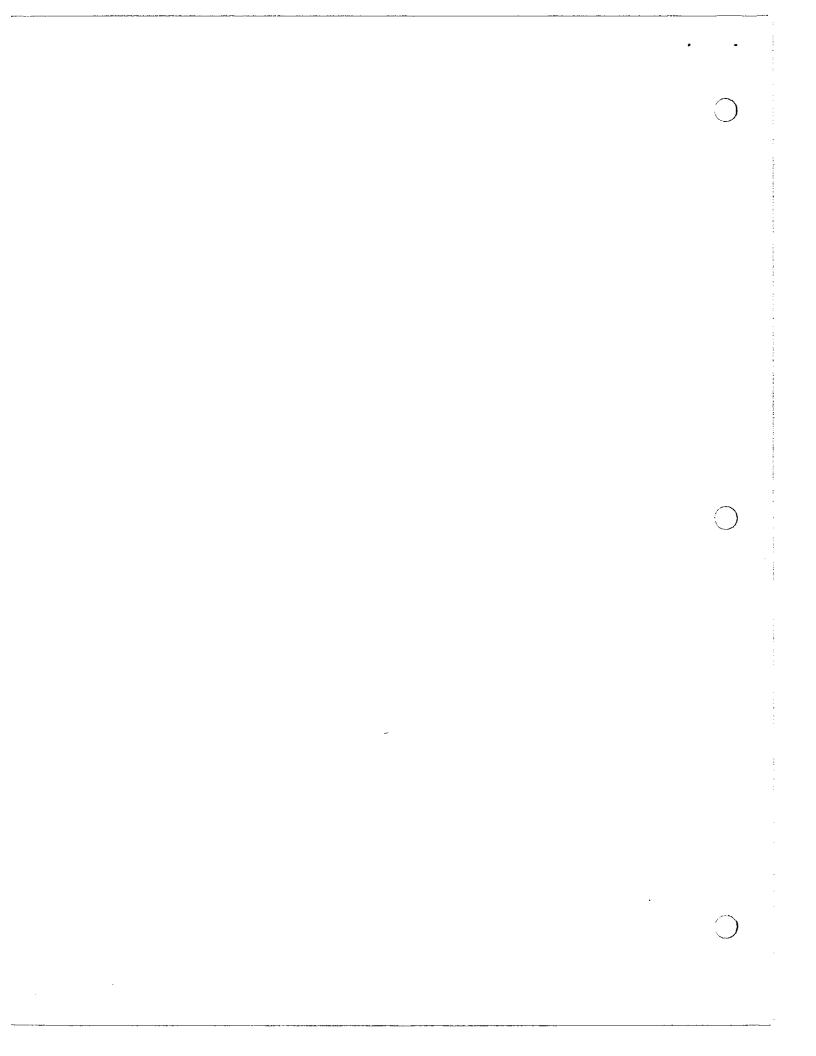
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NOAA NWSTM PR-19

CORRECTION SHEET TO NOAA TECHNICAL MEMO

"A Program to Compute Turbulence in the Vicinity of Lee Waves Downstream of Selected Mountains in the Hawaiian Islands"

- 1. In equations (7), (8), and (9): change h to a.
- 2. Page 2, para 2, 4th line: Change equation to: $\ell_1^2 \ell_2^2 > \pi^2/4h^2$.
- 3. Page 3, para 2, 2nd line: Change equation to: $\pi^2/4h^2$,
- 4. Page 3, para 2, 8th line: Change sentence to read:flow, a is height of mountain above the terrain, b is the half width of the mountain....
- 5. Page 3 para 2, 10th line: Change sentence to read:at distance x from the crest of the mountain ridge and h is the mountain height above sea level, $\rm U_1$ is the wind....
- 6. Page 5, para 2, 11th line: Insert the following sentence ahead of "The following table applies".

a is determined by substracting p from h.

7. Page 5, Table 1: Change column h to a. Change values under column a to:

Koolaus/NE 692 m Koolaus/SW 692 m Mt. Kaala/SW 830 m Mt. Haleakala/W 2559 m

8. Page 12: Change line 1190 LET H=814 to 1190 LET H=692

1220 LET H=814 to 1120 LET H=692

1250 LET H=1104 to 1250 LET H=830

1280 LET H=2803 to 1280 LET H=2559

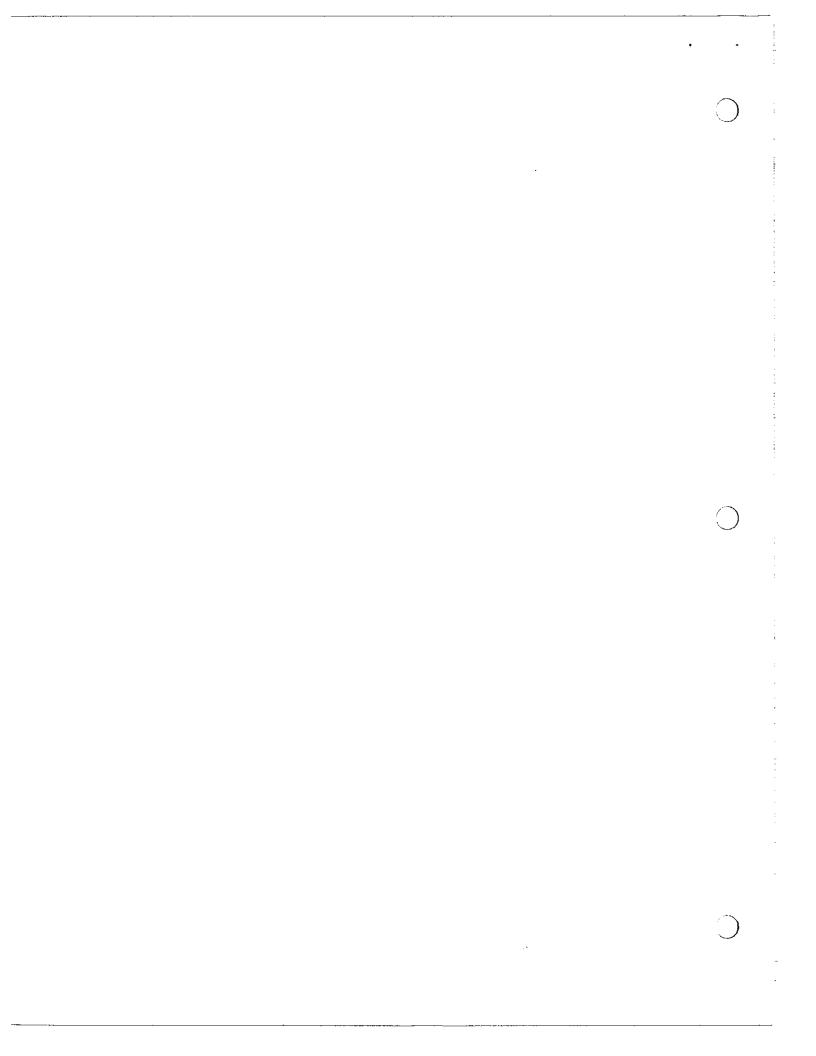
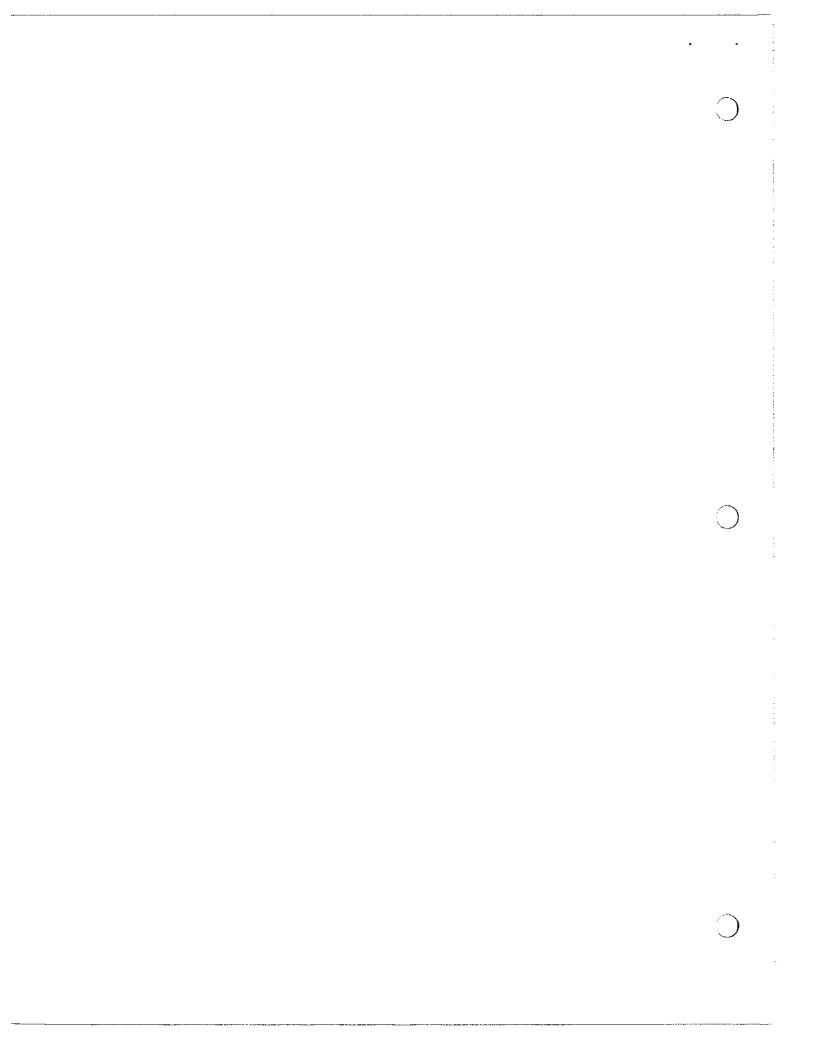


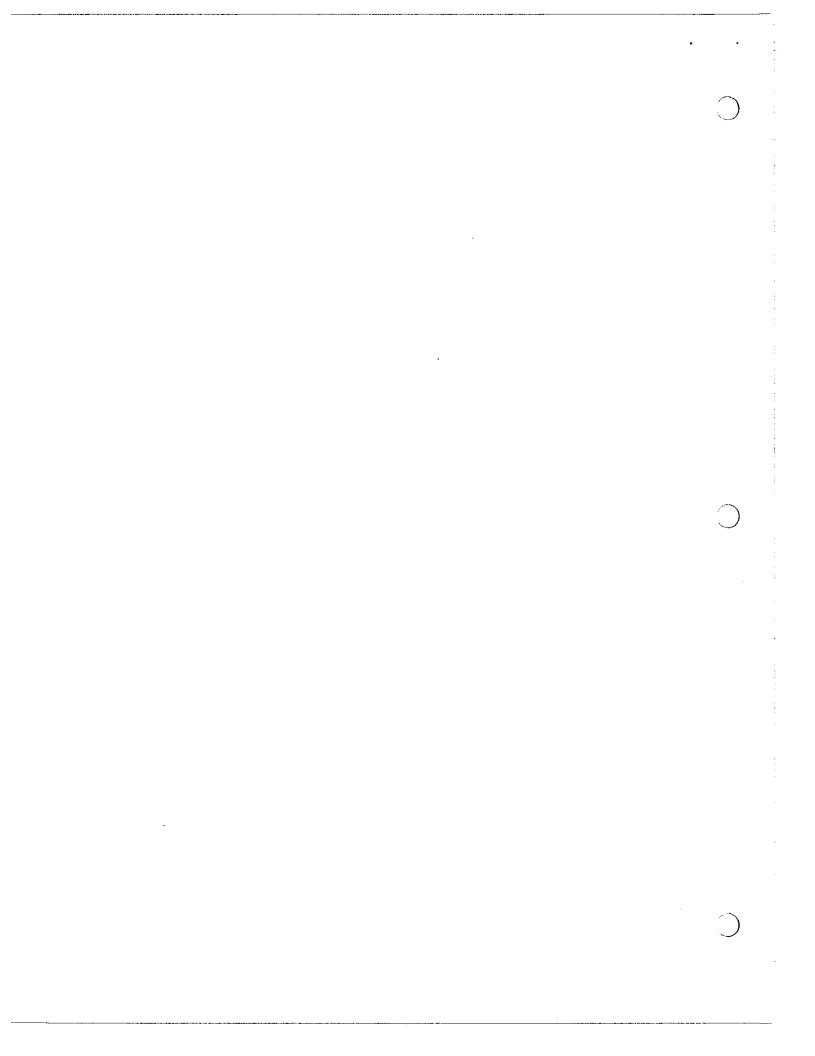
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ABSTRACT

With the advent of the geosynchronous satellite mountain wave clouds have become visible downstream of several islands in the Hawaiian Island chain. Turbulence associated with these waves poses a threat to aviation safety. This paper reviews the theory of lee wave formation and several applications of that theory with a view to now-casting turbulence categories associated with the waves in the Hawaiian chain. A computer program for minicomputers is described and suggestions for further study are made.



I. INTRODUCTION AND HISTORY

Since data from the SMS-2 satellite became available, mountain wave clouds have been visible downstream of the Koolaus on Oahu and occasionally down-stream of mountain ranges on Kauai, Molokai and Maui. Burroughs and Larson (1978) have documented a couple of well-defined cases of lee waves downstream of the Koolaus on Oahu. Subsequently a paper by Reiter and Foltz (1967) came to light which related the upward vertical motion found in lee waves to documented turbulence reported by specially instrumented planes. Using their formulations it is possible to get a quantitative feel for the actual turbulence in lee waves. Corby and Wallington's (1956) application of Scorer's theories (1949), (1953), (1954) was, also studied, and this resulted in the development of a computer program called TURBULENCE. It is designed to compute categories of turbulence in the vicinity of lee waves forming downstream of the Koolaus on the island of Oahu when winds are from the NE or SW quadrants, of Mt. Kaala on the island of Oahu when winds are from the SW quadrant, and of Mt. Haleakala on the island of Maui when winds are from the W quadrant. A program listing and a sample for NE winds are included as Appendices.

II. THEORY

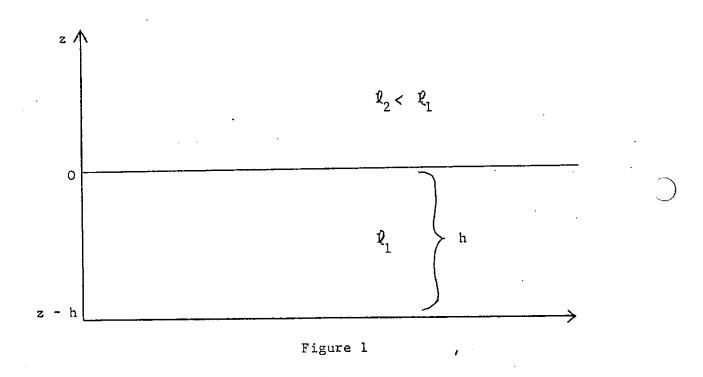
Scorer (1949) develops his theory utilizing dry, invicid, and isentropic stream flow in which there is a small proportionate disturbance of the wind velocity. He uses a two-layer model in which ψ is a stream function with a small disturbance caused by a mountain. The equation of motion is given by

$$\partial^{2}\psi/\partial Z^{2} - (gc^{-2} + Sg^{-1})\psi + (SU^{-2} - (\partial^{2}U/\partial Z^{2})U^{-1} - k^{2})\psi = 0$$
 (1)

where
$$\ell^2 = SU^{-2} - (\partial^2 U/\partial Z^2)U^{-1}$$
 is the Scorer parameter, (2)

 $S=g\theta^{-1}(\partial\theta/\partial Z)$ is the static stability, and U is the wind speed normal to the mountain range. k is the wave number in 2π unit distances in a direction perpendicular to the axis of the mountain range.

Fig. 1 shows the diagram of Scorer's two-layer model to solve the lee wave problem. The horizontal direction is taken normal to the axis of the mountain range positive downstream of the range.



For waves to form $\ell_1^2 - \ell_2^2 > \pi/4h^2$. Since the second term on the right side of (2) above is not important above the friction layer (900 m), it can normally be deleted; therefore,

$$\ell^2 = SU^{-2} \tag{3}$$

and the wavelength is given by

$$\lambda = 2\pi \ell^{-1} = 2\pi U S^{-1/2}$$
 (4)

Corby and Wallington (1956) have shown that a spectrum of wavelengths occurs

in mountain wave events, but the largest wavelength corresponding to the smallest wave number, k, dominates the flow and lies between ℓ_1 and ℓ_2 ; therefore, they theorize

$$k^2 = \ell_2^2 + L^2 \cos \alpha \tag{5}$$

where $L^2 = \ell_1^2 - \ell_2^2$ and k is the actual wave number measured from satellite imagery, for example. The boundary height is given by

$$h = (n\pi - \alpha)/L\sin\alpha \quad n=1, 2, 3, \dots$$
 (6)

Generally n is taken to be 1 since all parameters describing the lee waves are maximized for n = 1.

According to Corby and Wallington (1956), the most favorable conditions for wave formation are when L^2 is slightly greater than π^74h^2 , when L is large and when ℓ_2^2 is small. However, Scorer (1954) points out that even if these criteria are not met or ℓ_2 is not less than ℓ_1 , waves may form if an inversion is present. Corby and Wallington's (1956) solution to (1) is given by

$$\mathcal{E}_{z} = [-2 \pi hb/\exp(kb)] \left(U_{1}/U_{z} \right) \psi_{z,k} \left(\partial \psi_{1,k}/\partial k \right) \sin kx \tag{7}$$

where \mathcal{F}_z is the deviation of a streamline at level z from undisturbed flow, \mathbf{R} is height of the mountain, b is the half width of the mountain determined from $\rho = hb^2/(b^2+x^2)$ where ρ is the height of the terrain and has height of hornation at distance x from the crest of the mountain ridge, \mathbf{U}_1 is the wind above terrain component normal to the mountain crest at gradient level, \mathbf{U}_z is the wind component normal to the mountain crest at level z, $\psi_{z,k}$ is the stream function at level z for wave number k, and $\psi_{1,k}$ is the stream function at gradient level for wave number k.

The upward maximum vertical motion is given by

$$w = U_z(\partial_z^O/\partial x)_{max} = [-20 \text{Mb/exp(kb)}] U_1 a_n k$$
 (8)

where

$$a_n = \psi_{z,k} (\partial \psi_{1,k} / \partial k)^{-1} = \text{amplitude factor}$$

After some re-arranging and further work, Reiter and Foltz (1967) derived the following formulation of (7) for the vertical motion in mountain waves.

$$w_{o} = -(2\pi k_{0} + \exp(kb))U_{1}L^{2}(\sin^{2}\alpha/(n\pi - \alpha + \tan\alpha)).$$
 (9)

III. APPLICATION

Alaka (1960) showed

$$\lambda = 2\pi \overline{U}/\overline{S}^{\frac{1}{2}} \tag{10}$$

where the bars indicate averages over large depths in the atmosphere. Since \overline{S} is difficult to calculate, but \overline{U} is relatively easy to calculate, \overline{S} is derived using the following

$$\overline{S} = 4\pi^2 \overline{U}^2 \lambda^{-2} \tag{11}$$

where \overline{U} is the average wind component normal to the mountain range from the pibal level nearest the crest to the pibal level where the wind maximum occurs, λ is the wavelength measured from the satellite imagery.

Next l_1^2 and l_2^2 are calculated using the wind at the crest and the maximum wind. These are used to determine L^2 , then α is determined by re-arranging equation (5) such that

$$\alpha = \arccos(c) \text{ where } c = (k^2 - \ell_2)L^{-2}$$
 (12)

but since the mini-computer available doesn't have an inverse cosine function, an identify utilizing the inverse tangent function is used instead. Therefore,

$$\alpha = \arctan [(c^{-1})(1-c^2)^{\frac{1}{2}}]$$
 (13)

The wave number, k, is determined using

$$k = 2\pi\lambda^{-1} \tag{14}$$

where λ is the measured wavelength.

Four sets of mountain parameters have been determined using $\rho = hb^2(b^2+x^2)^{-1} \colon \text{a set for the Koolaus for trade conditions which applies only to the portion of the range not windward of the Waianaes, a set for the Koolaus for SW winds which applies to the portion of the range not leeward of the Waianaes, a set for Mt. Kaala for SW winds, and a set for Mt. Haleakala for W winds. The distance x was chosen to be the distance at which the slope became appreciably more gentle than that for the mountain range itself. Only in the case of a SW wind over the Koolaus would the results be materially changed by changing x. The effect would be to reduce the turbulence forecast and underforecast$

The effect would be to reduce the turbulence forecast and underforecast it. The following table applies.

RANGE/WIND	Ъ	H	ρ	х	
Koolaus/NE	3379m	814m	400ft	5mi	
Koolaus/SW	756m	-814m	400ft	1800m	
Mt. Kaala/SW	3702m	1104m 830	900ft	4mi	
Mt. Haleakala/W	4576m	2803m	8 00ft	8nm	

Table 1. Parameters defining the equivalent mountain used in determining upward vertical motion in the lee waves.

Reiter and Foltz (1967) developed a nomograph which gives estimated Clear Air Turbulence intensity levels. In order to develop equations for the curves in the nomograph curve fitting was done using cubic equations. The fitted equations are given below.

$$W_1 = 4.7451 \times 10^{-4 \lambda^3} - 2.5353 \times 10^{-2 \lambda^2} + 0.448 \lambda + 0.576$$
 (15)

$$W_2 = 1.3333 \times 10^{-4} \lambda^3 - 1.0 \times 10^{-2} \lambda^2 + 0.386 \lambda + 1.0,$$
 (16)

$$W_3 = 2.5297 \times 10^{-3} \lambda^3 - 9.1369 \times 10^{-2} \lambda^2 + 1.24 \lambda + 1.0$$
 (17)

where $W_{1,2,3}$ are in msec⁻¹ and λ is in km. W_1 defines a line separating categories of light and light to moderate turbulence; W_2 defines a line separating categories of light to moderate and moderate to severe turbulence; W_3 defines a line separating categories of moderate to severe and severe turbulence. W_0 is then compared to $W_{1,2,3}$ and the resulting category of turbulence is outputted to the user.

IV. RESULTS AND PROBLEMS

In general, the results seem reasonable; however, in the trade wind situation the maximum wind generally occurs below the trade inversion, and the values outputted appear low. Calculated values may indicate light turbulence when, in fact, it's reported to be moderate. This may be due to a variety of reasons including errors in the data or data not being representative—How good are Wheeler soundings? Do Lihue soundings represent the air mass over Oahu? Are the Honolulu pibals representative?—the way S, ℓ_1^2 , ℓ_2^2 are calculated and the neglect of $(\partial^2 U/\partial Z^2)U^{-1}$ in (2). Errors due to these factors appear to account for about 20 percent.

V. NOTABLE MISCELLANY

During trade wind situations two wind maxima are often apparent: one associated with the northeasterly winds in the lower half of the troposphere, and the other associated with the westerly winds in the upper half of the troposphere with a minimum and wind reversal between. Under these circumstances the number of wind velocities inputted include only those from the crest of the ridge to the first maxima.

In the few cases examined it has been noted that the criteria ${\rm L}^2$ > ${\pi/4h}^2$ has not been met whenever a strong inversion exists, even though waves have been evident. Scorer (1954) notes an inversion alters the criteria for wave formation. To overcome this problem somewhat and to account for the errors previously discussed, the criteria has been altered to $L^2 > 0.9\pi/4h^2$, and a question has been added to help the forecaster decide whether or not to go on. Scorer (1953), (1954) has pointed out several other interesting facts which help to explain what is often seen in the SMS-2 imagery at Honolulu. There is a diurnal variation in wavelength which occurs and may explain why (especially during trade conditions) the waves disappear in the afternoon. l^2 is reduced after sunrise and increased after sunset due to heating and decreasing stability. As the day progresses the wavelength increases until it essentially becomes infinite, i.e., there is no wave, and the criteria $L^2 > \pi/4h^2$ is no longer met. They tend to reappear at dusk. Waves occurring downstream of a single peak have shorter wavelengths and less turbulence than those downstream of an "infinite ridge". The persistence downstream of waves is greater the longer the ridge. The longer the wavelength is; the greater the amplitude is. Also narrower, steeper obstructions induce greater amplitudes (that's why the SW flow over the Koolaus on the island of Oahu can be so dangerous; the amplitude of the waves created is greater; and therefore, the turbulence is greater). Where a temperature inversion exists, the maximum amplitude of the waves will occur below the inversion. Where the amplitude is greatest is where the shear is greatest; and, hence, the turbulence is greatest (Pao and Goldburg, 1969).

VI. SUGGESTED PROJECTS

Several projects which would improve and expand the program's capabilities follow. Lee waves tend to damp out downstream, and a regression equation relating the number of waves downstream to the average wind speed normal to the ridge from the crest of the ridge to the wind maximum should be derived. From this regression equation a damping function can be developed to show the forecaster how far downstream moderate of greater turbulence can be expected. There are days when conditions favorable to formation of lee waves exist, but wave clouds do not form due to lack of moisture or cannot be seen due to mid and high cloud interference. Here again a regression equation should be developed equating the wavelength to the average wind speed (defined above). In both derivations suggested, separate formulae should be developed for strong inversion situations where the speed maximum is below the inversion and for all other cases combined. It may be necessary to further stratify the data by wind direction. Once such regression equations exist, a shift from nowcasting to forecasting can be made because it will no longer be necessary to see wave clouds to do the calculations. The forecasts could then be refined by use of the satellite imagery. The program's utility may also be increased by adding mountain parameters for Kauai, Molokai and the combined effect of the Koolaus and Waianaes. Some means of making the Koolaus and Waianaes into an equivalent range needs to be studied before the latter can be done.

VII. ACKNOWLEDGMENTS

Special thanks are due Ms. Barbara Howerton for typing the manuscript and Prof. Wan-Cheng Chiu for reviewing it. His comments have been very helpful.

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PROGRAM LISTING

```
BASIC TURBULENCE
LIST
100 DIM X[25],T[25],S[25],A1[25]
      PRINT
               "THIS PROGRAM GIVES CATAGORIES OF TURBULENCE WHICH MAY" "BE EXPECTED IN THE VICINITY OF WAVES IN THE LEE OF" "MOUNTAIN RANGES OR INDIVIDUAL MOUNTAIN PEAKS. IT IS"
      PRINT
120
130 PRINT
140 PRINT
                "CURRENTLY VALID FOR THE KODLAUS WHEN WINDS ARE FROM"
150 PRINT
                "THE NE OR SW QUADRANTS, MT KAALA WHEN WINDS ARE FROM"
160 PRINT
170 PRINT
                "SW QUADRANT AND MT HALEAKALA WHEN WINDS ARE FROM THE"
                "W QUADRANT. THE INPUTS TO THE PROGRAM ARE THE NUMBER"
180 PRINT
               "OF PIBAL WINDS BETWEEN THE CREST OF THE MOUNTAIN"
"AND THE MAX WIND ABOVE THE CREST INCLUSIVE, THE WIND"
190
     PRINT
200 PRINT
               "DIRECTION AND SPEED AT EACH LEVEL, AND THE WAVELENGTH"
      PRINT
210
               "MEASURED AS THE NUMBER OF WAVES PER DISTANCE, IE USING"
"AT LEAST 5 WAVE CLOUDS MEASURE THE DISTANCE FROM FIRST"
220
     PRINT
230 PRINT
               "TO LAST WAVE AND INPUT THE NUMBER OF WAVES AND THE"
"DISTANCE MEASURED IN NAUTICAL MILES (NM). THE 3000FT"
     PRINT
240
     PRINT
250
               "WIND IS THE STARTING POINT FOR THE MOUNTAINS ON DAHU."
"WIND IS THE STARTING POINT FOR THE MOUNTAINS ON DAHU."
"THE 10000FT WIND OR WIND MEAREST TO THAT LEVEL ABOVE"
"THE SUMMIT OF HALEAKALA IS THE STARTING POINT ON MAUI."
"THE LAST WIND INPUTTED SHOULD ALWAYS BE THE MAX WIND."
"USE THE BEST WINDS AVAILABLE. YOU MAY USE UP TO 25"
"WIND VELOCITIES. USE KNOTS FOR ALL WIND SPEEDS."
"WHAT IS THE NUMBER OF WIND WELDCITIES YOU WISE TO USES"
260
270
280
      PRINT
     PRINT
      PRINT
290
      PRINT
300
310
      PRINT
                "WHAT IS THE MUMBER OF WIND VELOCITIES YOU WISH TO USE?"
32ŭ
      PRINT
330
340
      PRIMI
      IMPUT
350
     PRINT
360 PRINT
               "GIVE ME YOUR VELOCITIES AS DIRECTION, SPEED RETURN."
370
380
390
      PRINT
FOR I
         Ř Í=1 TO M
IMPUT XCII,TCII
         LET SIII=TIII+6080/(3600+3.2808)
400
410 MEXT
420 PRINT
430 PRINT "51VE ME NUMBER OF WAVES, DISTANCE MEASURED RETURN"
440 PRINT
450
      IMPUT
              N \cdot D
460 PRINT
470 LET W=D+6080/(N+3.2808)
            W=W/1000
480 LET
            W1=4.7451E-04+W+W+W-2.5353E-02+W+W+.448+W+.576
490
      LET
            W2=1.3333E-04*W*W+W-1E-02*W*W+.386*W+1
500
      LET
510 LET
            W3=2.5297E-03+W+W+W-9.1369E-02+W+W+1.24+W+1
520
            W=W+1000
      LET
530
      PRINT
540
      PRINT
               "GIVE ME WIND DIRECTION. IF HE QUAD TYPE 1, IF SW QUAD"
               "TYPE 2, IF WAVES APPEAR TO BE FORMING IN THE LEE OF MT"
550 PRINT
               "KAALA ONLY TYPE 3, IF W QUAD TYPE 4.
      PRINT
560
570 PRINT
580 IMPUT
590 IF Z=1 GOTO 630
600 IF Z=2 GOTO 730
610 IF Z=3 GOTO 730
620 IF Z=4 GOTO 830
630
     LET A2=0
```

```
640 LET P1=3.1415927
650 FOR I=1 TO M
660 LET X1= ABS (60-X[I])
670 LET Y=(90-X1)+F1/180
680 LET 04 SIN (Y)
                                          (60-X[I])
              LET A1[[]=S(i)+A
690
              LET A2=A2+A1[]]
700
710 NEXT I
720 GOTO 920
730 LET A2=0
740 LET P1=3.1415927
750 FOR I=1 TO M
760    LET X1= ABS (240-X[I])
770    LET Y=(270-X1)+P1/180
780    LET A= SIN (Y)
790    LET A1[I]=S[I]+A
800    LET A2=A2+A1[I]
810    NEXT I
820 GOTO 920
720 60TD
                       920
                                         (240-X[I])
810
820
                      <sup>1</sup>920
         60TO
        LET A2=0

LET P1=3.1415927

FOR I=1 TO M

LET X1= ABS (270-X[I])

LET Y=(270-X1)+P1/180

LET A= SIN (Y)
83ŏ
850 FOR
860 LE
870 LE
                                          (270-X[I])
880
              LĒĪ AICĪĪ=SCIĪ+A
890
900
970 LET A2=A2+
910 MEXT I
920 LET A2=A2/M
930 LET A3=A1[1]
940 LET A4=A1[M]
950 LET S1=4+P1+
                       A2=A2+A1[I]
                  S1=4+P1+P1+A2+A2/(W+W)
960 LET L3=S1/(A3+A3)
970 LET L4=S1/(A4+A4)
980 LET L2=L3-L4
990 LET L= SQR (L2)
1000 LET K2=4+P1+P1/(W+W)
1010 LET K= SQR (K2)
1020 LET C=(K2-L4)/L2
1030 LET C1= ATN ( SQR (1-C+C)/C)
1040 LET H1=P1-C1/(L+ SIN (C1))
1050 IF L2>.9+P1+P1/(4+H1+H1) GDTD
                                                                                     1150
           PRINT
1060
                        "CRITERIA FOR LEE WAVES HAS NOT BEEN MET. DO YOU WISH"
"TO CONTINUE THE CALCULATION. IF YES TYPE 1, IF NO TYPE"
"2. CONTINUE IF STRONG INVERSION EXISTS OR IF WAVE"
"CLOUDS ALREADY FXIST."
1070 PRINT
1080 PRINT
1090
           PRINT
           PRINT
                          "CLOUDS ALREADY EXIST.
1100
1110
           PRIMT
1120
            TURMI
1130
            IF R=1 GDTD
            IF
1140
                  R=2
                           60TO
                                          1770
                  Z=1 GOTO
Z=2 GOTO
Z=3 GOTO
Z=4 GOTO
                                          1190
1220
1250
            ÎF
1150
1160
            ĪF
1170
           ΙF
1180
                                          1280
           LET H=$14 692
LET B=3379
1190
1200
1210
1220
1230
           LET B=3379
GOTO 1300
LET H=814 692
LET B=756
           60TO 1300
1240
           LET H=1104 830
1250
1260
1270
1280
           LET B=3702
60T0 1300
LET H=2803
LET B=4576
```

```
1300 LET P=2+P1+H+B+A1[1]+L2+ SIN (C1)+ SIN (C1)
1310 LET Q= EXP (K+B)+(P1-C1+ TAN (C1))
1320 LET WO= ABS (-P/Q)
1330
       IF WO<W1 GOTO 1440
1340 IF W0>=W1 IF W0<W2 60T0
1350 IF W0>=W2 IF W0<W3 60T0
                                           1500
1360 LET C2=C1+180/P1
1370 PRINT
               "CALCULATION INDICATES SEVERE TURBULENCE PRESENT."
"RECOMMEND SIGNET BE ISSUED. MAX TURBULENCE WILL OCCUR"
"BELOW INVERSION IF PRESENT AND IN THE FIRST FEW WAVES"
"NEAREST CREST OF RIDGE. IF NO INVERSION PRESENT MAX"
1380 PRINT
1390 PRINT
1400 PRINT
1410 PRINT
               "TURBULENCE WILL OCCUR BELOW LEVEL OF WAVE CLOUD TOPS."
1420 PRINT
1430 GOTO 1660
1440 PRINT
               "CALCULATION INDICATES LIGHT TURBULENCE OR LESS PRE—"
"SENT VICINITY WAVE CLOUDS. UNLESS OTHER DATA INDICATE"
"TURBULENCE OF A HIGHER CATAGORY. RECOMMEND NO AIRMET"
"BE ISSUED."
1450 PRINT
1460 PRINT
1470 PRINT
1480 PRINT
1490 GOTO 1660
1500 PRINT
               "CALCULATION INDICATES LIGHT TO MODERATE TURBULENCE"
"PRESENT VICINITY WAVE CLOUDS. RECOMMEND WIRMET BE"
"ISSUED. MAX TURBULENCE WILL OCCUR BELOW INVERSION IF"
"PRESENT AND IN THE FIRST FEW WAVES CLOSEST TO THE"
1510 PRINT
1520 PRINT
1530 PRINT
1540 PRINT
               "CREST OF THE RIDGE. IF NO INVERSION PRESENT MAX TUR-"
1550 PRINT
               "BULENCE WILL OCCUR BELOW LEVEL OF WAVE CLOUD TOPS."
1560 PRINT
1570 GOTO_1660
      PŘÍŇT
PRINT
1590
                 CALCULATION INDICATES MODERATE TO SEVERE TURBULENCE"
                "PRESENT VICINITY WAVE CLOUDS. RECOMMEND AIRMET BE"
1600 PRINT
                "ISSUED UNLESS OTHER DATA INDICATES A SIGMET IS RE-"
1610 PRINT
                "QUIRED. MAX TURBULENCE WILL OCCUR BELOW INVERSION IF"
1620 PRINT
               "PRESENT AND IN THE FIRST FEW WAVES CLOSEST TO THE"
"CREST OF THE RIDGE. IF NO INVERSION PRESENT MAX TUR-"
"BULENCE WILL OCCUR BELOW LEVEL OF WAVE CLOUD TOPS."
1630 PRINT
1640 PRINT
1650 PRINT
1660 PRINT
1670 PRINT
                "ALL OUTPUT VALUES ARE IN M.K.S. UMITS."
1680 PRINT
                "THE ABSOLUTE VALUE OF VERTICAL WIND SPEED = "WO;" M/S"
1690 PRINT
1700 PRINT
î7ĭŏ PRÎNT
                "AVERAGE NORMAL WIND SPEED = "A2;" M/S"
1720 PRINT
       PRINT
                "AVERAGE STATIC STABILITY = "S1
1730
       PRINI
PRINI
1740
1750
                "WAVELENGTH = "W;" M"
       FRINT
                "DO YOU WISH TO CONTINUE? IF YES TYPE 1 IF NO TYPE 2."
1780 PRINT
1790
       INPUT
1800
1810
1820
1830
       PRINT
IF G=
       TF 6=1 GOTO
CHAIN "GOTO
STOP
END
                          320
1840
```

APPENDIX II

SAMPLE OUTPUT

STURBULENCE

THIS PROGRAM GIVES CATAGORIES OF TURBULENCE WHICH MAY BE EXPECTED IN THE VICINITY OF WAVES IN THE LEE OF MOUNTAIN RANGES OR INDIVIDUAL MOUNTAIN PEAKS. IT IS CURRENTLY VALID FOR THE KOOLAUS WHEN WINDS ARE FROM THE NE OR SW QUADRANTS, MT KAALA WHEN WINDS ARE FROM THE NE OR SW QUADRANT AND MT HALEAKALA WHEN WINDS ARE FROM THE WOUNDAMN. THE INPUTS TO THE PROGRAM ARE THE NUMBER OF PIBAL WINDS BETWEEN THE CREST OF THE MOUNTAIN AND THE MAX WIND ABOVE THE CREST INCLUSIVE, THE WIND DIRECTION AND SPEED AT EACH LEVEL, AND THE WAVELENGTH MEASURED AS THE NUMBER OF WAVES PER DISTANCE, IE USING AT LEAST 5 WAVE CLOUDS MEASURE THE DISTANCE FROM FIRST TO LAST WAVE AND INPUT THE NUMBER OF WAVES AND THE DISTANCE MEASURED IN MAUTICAL MILES (MM). THE 3000FT WIND IS THE STARTING POINT FOR THE MOUNTAINS ON OAHU. THE 10000FT WIND OR WIND MEAREST TO THAT LEVEL ABOVE THE SUMMIT OF HALEAKALA IS THE STARTING POINT ON MAUI. THE LAST WIND INPUTTED SHOULD ALWAYS BE THE MAX WIND. USE THE BEST WINDS AVAILABLE. YOU MAY USE UP TO 25 WIND VELOCITIES, USE KNOTS FOR ALL WIND SPEEDS. WHAT IS THE NUMBER OF WIND VELOCITIES YOU WISH TO USE?

? 3 GIVE ME YOUR VELOCITIES AS DIRECTION, SPEED RETURN.

? 080,25? 075,35? 075,36 GIVE ME NUMBER OF WAVES, DISTANCE MEASURED RETURN

7 6,35.4

GIVE ME WIND DIRECTION. IF NE QUAD TYPE 1, IF SW QUAD TYPE 2, IF WAVES APPEAR TO BE FORMING IN THE LEE OF MT KAALA ONLY TYPE 3, IF W QUAD TYPE 4.

? 1 CRITERIA FOR LEE WAVES HAS NOT BEEN MET. DO YOU WISH TO CONTINUE THE CALCULATION. IF YES TYPE 1, IF NO TYPE 2. CONTINUE IF STRONG INVERSION EXISTS OR IF WAVE CLOUDS ALREADY EXIST.

? 1 CALCULATION INDICATES LIGHT TURBULENCE OR LESS PRE-SENT VICINITY WAVE CLOUDS. UNLESS OTHER DATA INDICATE TURBULENCE OF A HIGHER CATAGORY. RECOMMEND NO AIRMET BE ISSUED.

ALL BUTPUT VALUES ARE IN M.K.S. UNITS.

THE ABSOLUTE VALUE OF VERTICAL WIND SPEED = 1.47146 M/S

AVERAGE NORMAL WIND SPEED = 15.7989 M/S

AVERAGE STATIC STABILITY = 8.24256E-05

WAVELENGTH = 10933.9 M

DO YOU WISH TO CONTINUE? IF YES TYPE 1 IF NO TYPE 2.